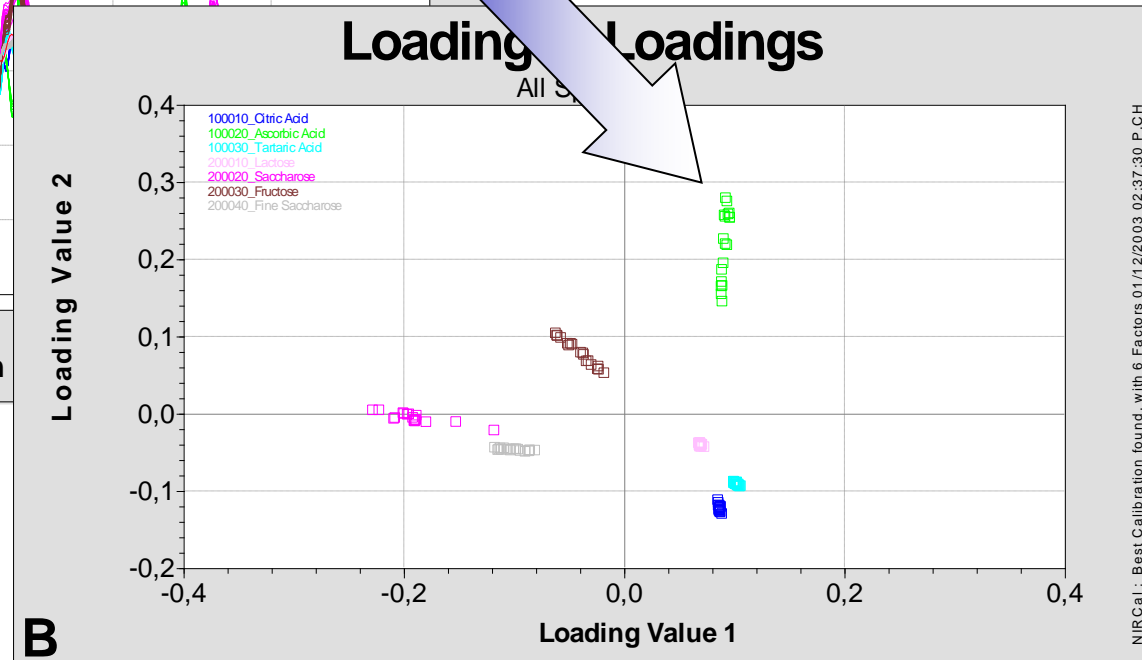
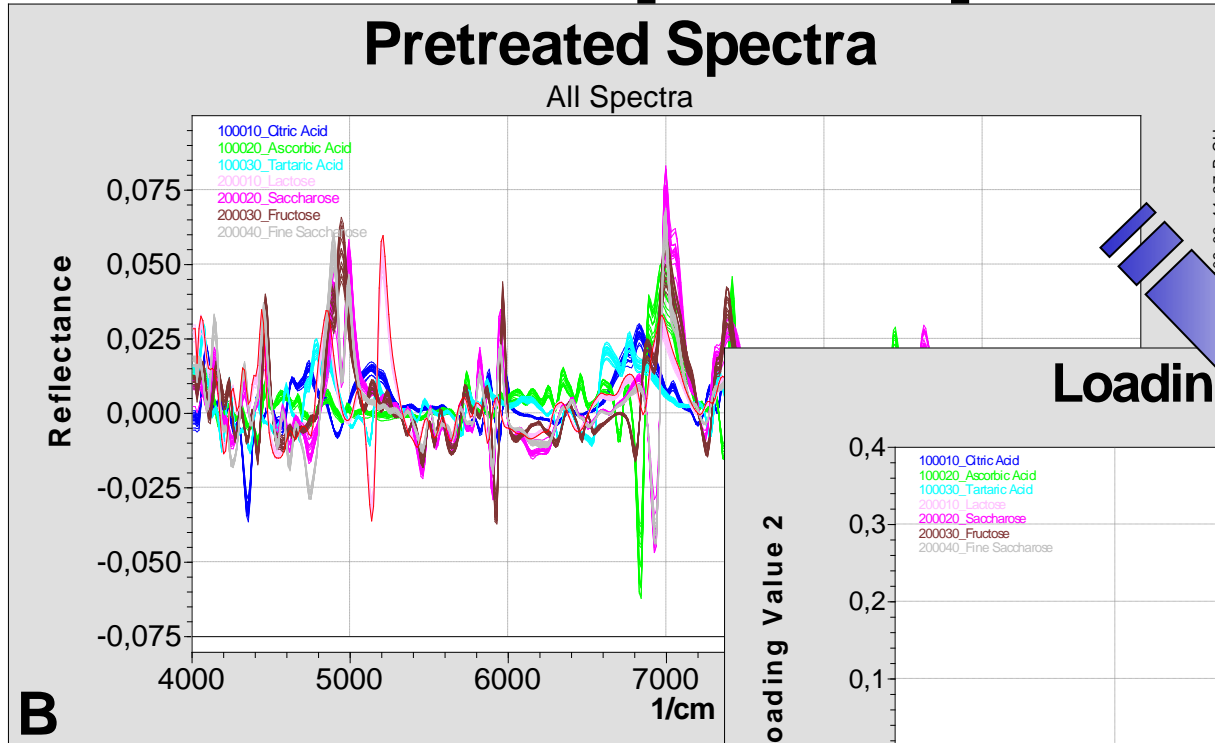


# Analyse en composantes principales



# Présentation

- L'ACP permet de réduire un système complexe de corrélations à un plus petit nombre de dimensions.
- Permet de générer des variables latentes non corrélées

# Données de départ

- Des individus caractérisés par un certain nombre de variables
  - Laquelle est la plus importante pour caractériser les individus ?
  - Sont elles toutes pertinentes et/ou corrélées ?

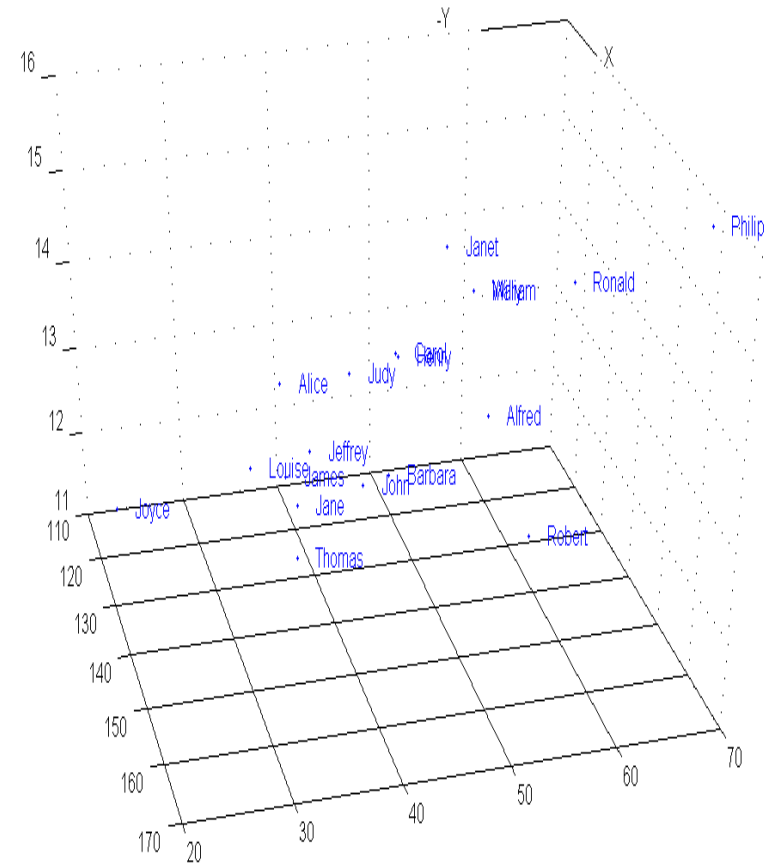
| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  | 155    | 51    | 14  |
| Alice   | 124    | 38    | 13  |
| Barbara | 146    | 44    | 13  |
| Carol   | 140    | 46    | 14  |
| Henry   | 141    | 46    | 14  |
| James   | 126    | 38    | 12  |
| Jane    | 132    | 38    | 12  |
| Janet   | 139    | 51    | 15  |
| Jeffrey | 139    | 38    | 13  |
| John    | 130    | 45    | 12  |
| Joyce   | 110    | 23    | 11  |
| Judy    | 143    | 41    | 14  |
| Louise  | 123    | 35    | 12  |
| Mary    | 149    | 51    | 15  |
| Philip  | 163    | 68    | 16  |
| Robert  | 145    | 58    | 12  |
| Ronald  | 150    | 60    | 15  |
| Thomas  | 126    | 39    | 11  |
| William | 149    | 51    | 15  |

# Corrélations

- Les 3 variables sont dépendantes les unes des autres.

|        | TAILLE  | POIDS   | AGE |
|--------|---------|---------|-----|
| TAILLE | 1       |         |     |
| POIDS  | 0,87779 | 1       |     |
| AGE    | 0,81143 | 0,74089 | 1   |

- La situation n'est peut être pas si compliquée.

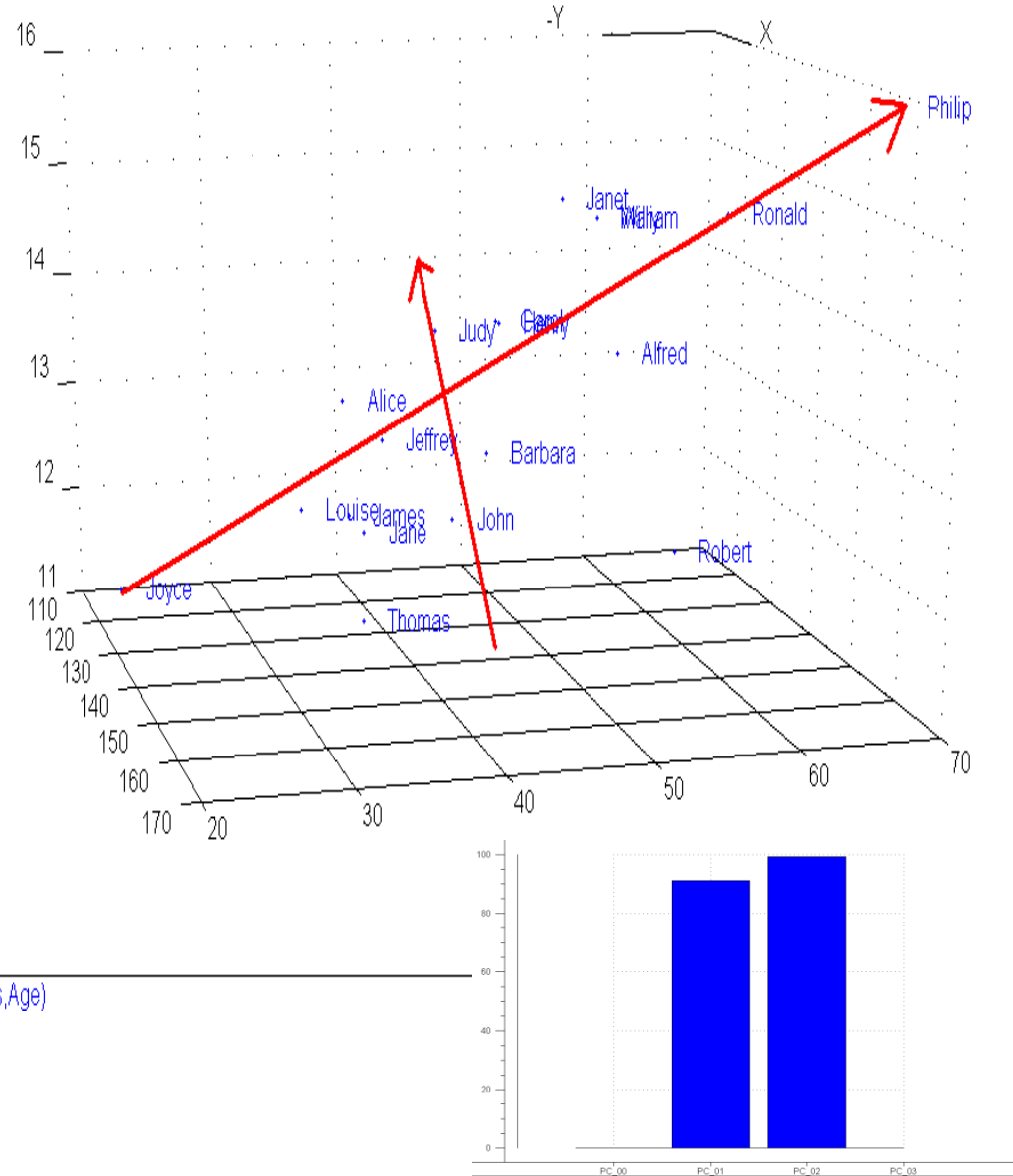


# Que fait l'ACP ?

- Calcul de nouvelles variables: les composantes principales.
  - Géométriquement,
    - on cherche le plus grand sens d'élongation du nuage de point (CP N°1)
    - Puis, le second (CP N°2)
  - Et on regarde le pourcentage de variance « expliqué » par ces axes (variables)
 

|          |     |
|----------|-----|
| • PC 1   | 91% |
| • PC 1+2 | 99% |

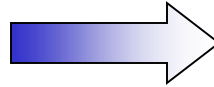
(Taille,Poids,Age)



# Le calcul...

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  | 155    | 51    | 14  |
| Alice   | 124    | 38    | 13  |
| Barbara | 146    | 44    | 13  |
| Carol   | 140    | 46    | 14  |
| Henry   | 141    | 46    | 14  |
| James   | 126    | 38    | 12  |
| Jane    | 132    | 38    | 12  |
| Janet   | 139    | 51    | 15  |
| Jeffrey | 139    | 38    | 13  |
| John    | 130    | 45    | 12  |
| Joyce   | 110    | 23    | 11  |
| Judy    | 143    | 41    | 14  |
| Louise  | 123    | 35    | 12  |
| Mary    | 149    | 51    | 15  |
| Philip  | 163    | 68    | 16  |
| Robert  | 145    | 58    | 12  |
| Ronald  | 150    | 60    | 15  |
| Thomas  | 126    | 39    | 11  |
| William | 149    | 51    | 15  |

Matrice X



| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

Matrice Xc  
centrée sur la  
moyenne  
variable par  
variable

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$X_C$

=

$P_1^T$

| Taille  | Poids | Age |
|---------|-------|-----|
| Alfred  |       |     |
| Alice   |       |     |
| Barbara |       |     |
| Carol   |       |     |
| Henry   |       |     |
| James   |       |     |
| Jane    |       |     |
| Janet   |       |     |
| Jeffrey |       |     |
| John    |       |     |
| Joyce   |       |     |
| Judy    |       |     |
| Louise  |       |     |
| Mary    |       |     |
| Philip  |       |     |
| Robert  |       |     |
| Ronald  |       |     |
| Thomas  |       |     |
| William |       |     |

$T_1$

**1ère composante**

+

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$R_1$

$$X_C = T_1 * (P_1)^T + R_1$$

# Le calcul est itératif

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$X_C$

=

|         |
|---------|
| Alfred  |
| Alice   |
| Barbara |
| Carol   |
| Henry   |
| James   |
| Jane    |
| Janet   |
| Jeffrey |
| John    |
| Joyce   |
| Judy    |
| Louise  |
| Mary    |
| Philip  |
| Robert  |
| Ronald  |
| Thomas  |
| William |

$T_1$

$\times$

| Taille | Poids | Age |
|--------|-------|-----|
|        |       |     |

$P_1$

+

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$R_1$

**1ère composante**

$$X_C = T_1 \cdot (P_1)^T + R_1$$

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$R_1$

=

|         |
|---------|
| Alfred  |
| Alice   |
| Barbara |
| Carol   |
| Henry   |
| James   |
| Jane    |
| Janet   |
| Jeffrey |
| John    |
| Joyce   |
| Judy    |
| Louise  |
| Mary    |
| Philip  |
| Robert  |
| Ronald  |
| Thomas  |
| William |

$T_2$

$\times$

| Taille | Poids | Age |
|--------|-------|-----|
|        |       |     |

$P_2$

+

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Alfred  |        |       |     |
| Alice   |        |       |     |
| Barbara |        |       |     |
| Carol   |        |       |     |
| Henry   |        |       |     |
| James   |        |       |     |
| Jane    |        |       |     |
| Janet   |        |       |     |
| Jeffrey |        |       |     |
| John    |        |       |     |
| Joyce   |        |       |     |
| Judy    |        |       |     |
| Louise  |        |       |     |
| Mary    |        |       |     |
| Philip  |        |       |     |
| Robert  |        |       |     |
| Ronald  |        |       |     |
| Thomas  |        |       |     |
| William |        |       |     |

$R_2$

**2nde composante**

$$R_1 = T_2 \cdot (P_2)^T + R_2$$

$$R_{n-1} = T_n \cdot (P_n)^T + R_n$$

# Le calcul conduit a:

- Une modélisation des données par
  - Un ensemble de CP (T et P) qui
    - contiennent une part décroissante d'information
      - Importante pour les premières composantes
      - Mineure pour les dernières
    - Ne sont pas corrélées (sont indépendantes les unes des autres)
- Les loadings représentent le « poids » des variables de départ dans chaque composante
- Les scores représentent la position des individus sur chacune des composantes

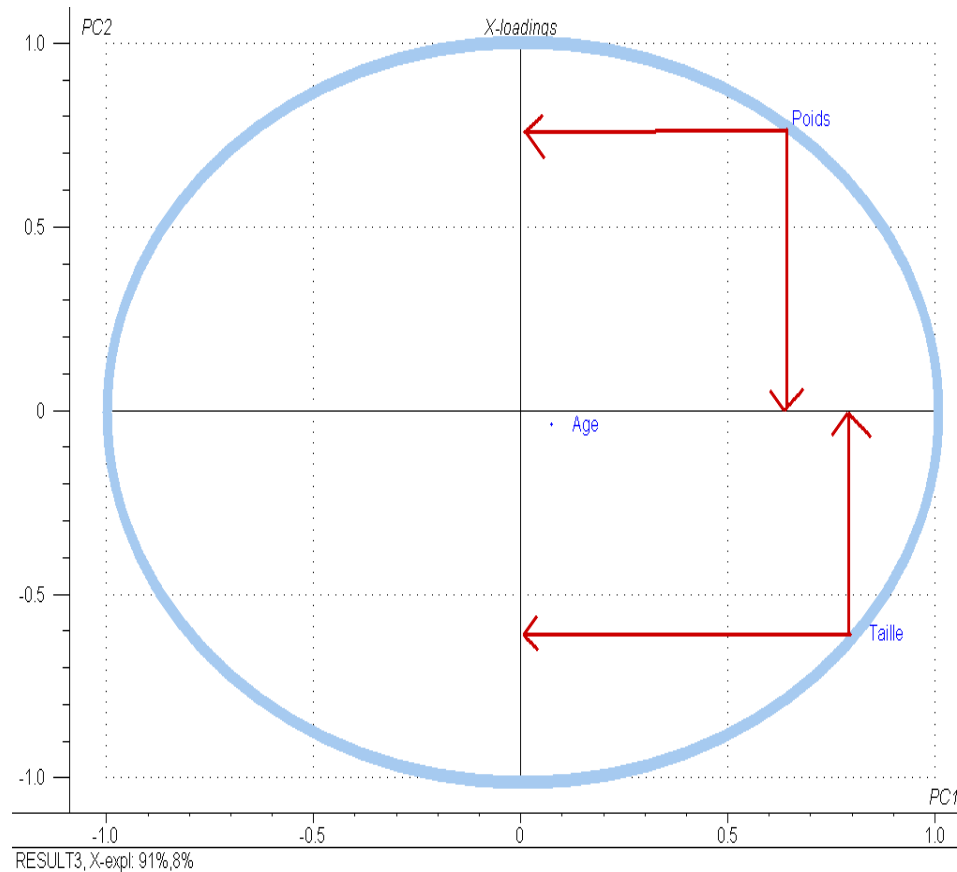


# Dans la pratique

- Le calcul s'effectue par minimisation de la SCE pour calculer scores et loadings à chaque étape.
- Une fraction des individus doit être laissée en dehors du processus de calcul pour vérifier la convergence de l'algorithme « **validation set** »
- Les individus qui servent au calcul correspondent au « **calibration set** »
- Face à un petit nombre d'individus, on peut utiliser la technique de « **cross validation** » ou « leave one out ».

# Loading plot

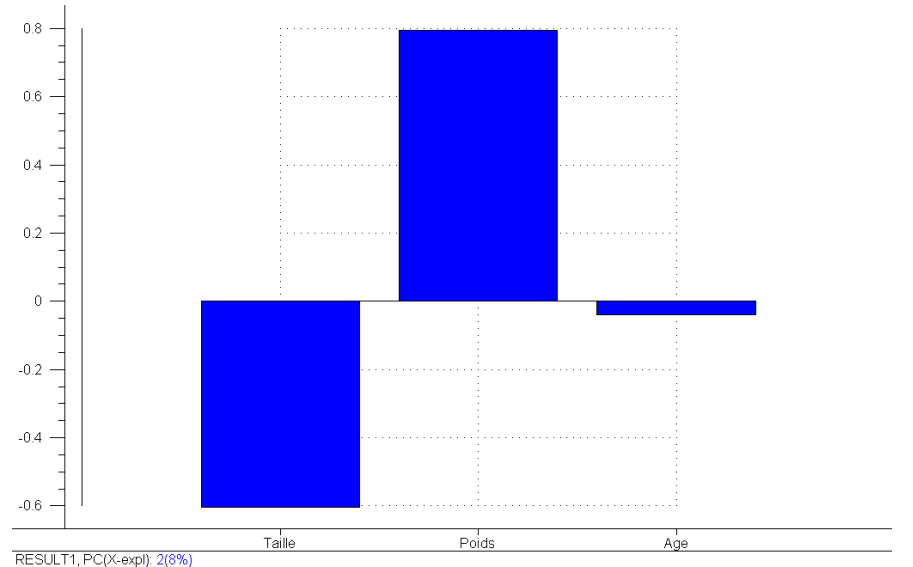
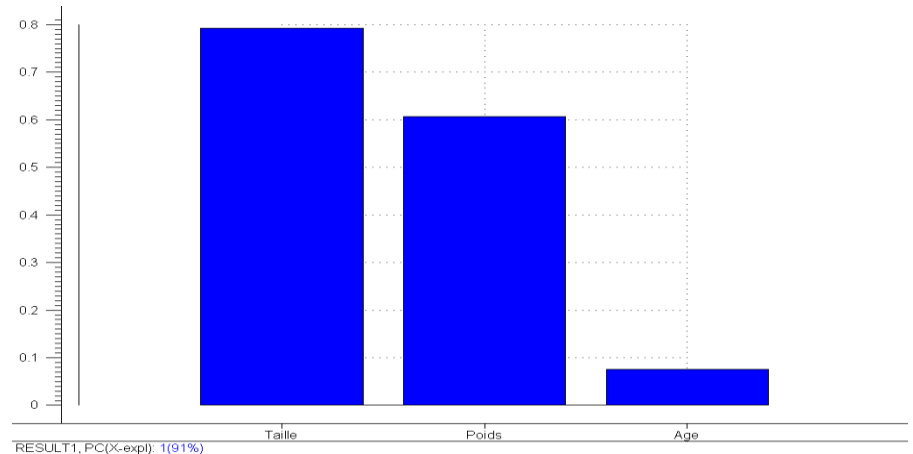
- Positionne les variables d'origine dans le nouveau système
  - Ici, on « voit » 99% des données
  - La taille est la variable qui corrèle le plus avec le nouvel axe. L'axe 1 contient aussi l'information « poids ».
  - L'axe 2 oppose taille/poids
  - L'âge ne semble pas être un critère pertinent pour décrire nos individus



# Corrélations.

|        | TAILLE  | POIDS   | AGE |
|--------|---------|---------|-----|
| TAILLE | 1       |         |     |
| POIDS  | 0,87779 | 1       |     |
| AGE    | 0,81143 | 0,74089 | 1   |

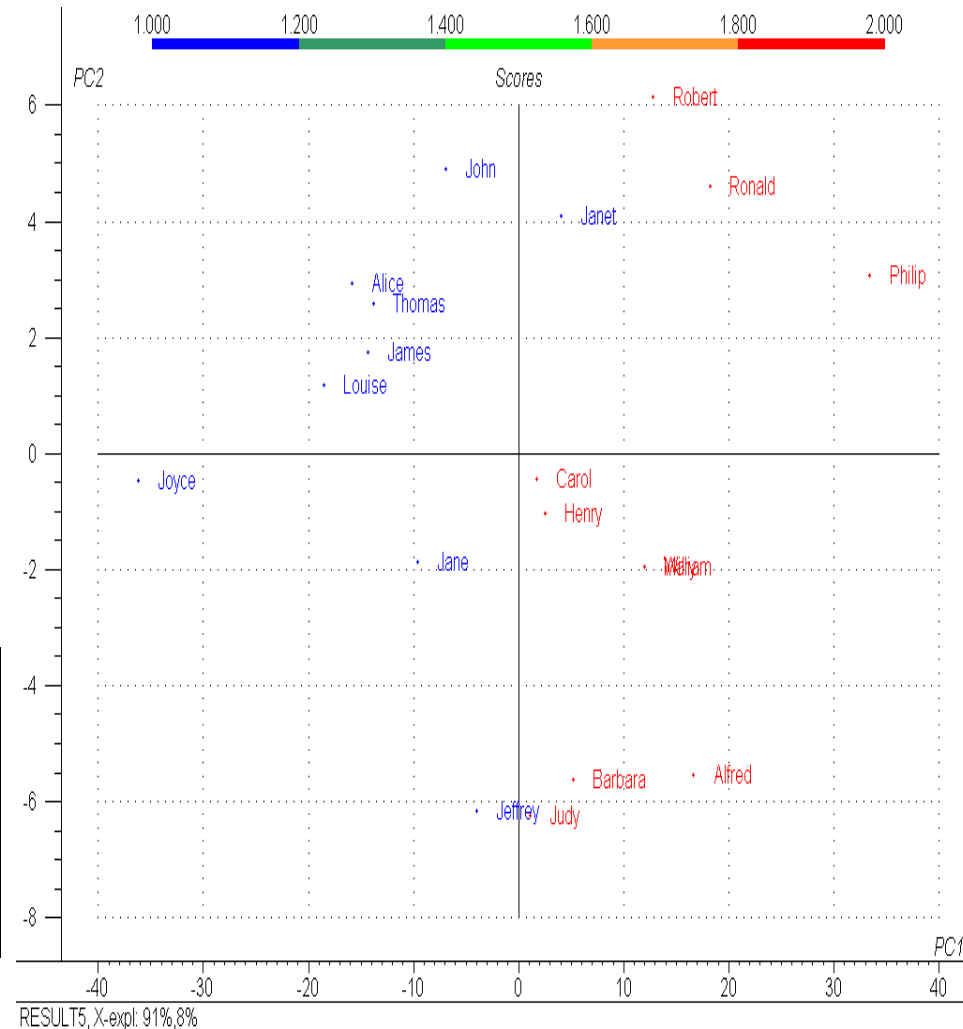
- On retrouve la corrélation taille-poids sur le loading 1
- Sur le 2 ces variables sont anticorrélées



# Score plot

- Les coordonnées de nos individus dans le système.
  - En rouge individus de taille  $\geq 1,40$  m
  - En bleu  $\leq 1,40$  m

| Prénom  | Taille | Poids | Age |
|---------|--------|-------|-----|
| Philip  | 163    | 68    | 16  |
| Robert  | 145    | 58    | 12  |
| Jeffrey | 139    | 38    | 13  |
| Joyce   | 110    | 23    | 11  |



# Exemple 1

- Développement de nanoparticules\* par voie orale pour un API faiblement hydrosoluble (telmisartan).
- \*Nanosuspension stabilisée par des surfactants
- Combinaison d'un plan factoriel et d'une ACP
- Plan:  $3^2$ 
  - X1 stabilisant %w/v
  - X2 agent de broyage en g
- Réponses:
  - Taille de particules
  - indice de polydispersité (PI)
  - Solubilité à saturation
  - Potentiel Zeta

**Table 1**

Design layout of  $3^2$  full factorial design batches for TLM loaded nanosuspensions.

| Batch code | Transformed values |         |
|------------|--------------------|---------|
|            | $X_1^a$            | $X_2^b$ |
| TLM-NS-F1  | -1                 | -1      |
| TLM-NS-F2  | -1                 | 0       |
| TLM-NS-F3  | -1                 | 1       |
| TLM-NS-F4  | 0                  | -1      |
| TLM-NS-F5  | 0                  | 0       |
| TLM-NS-F6  | 0                  | 1       |
| TLM-NS-F7  | 1                  | -1      |
| TLM-NS-F8  | 1                  | 0       |
| TLM-NS-F9  | 1                  | 1       |

Jaydeep Patel, Anjali Dhingani, Kevin Garala, Mihir Raval, Navin Sheth,  
 Design and development of solid nanoparticulate dosage forms of telmisartan for  
 bioavailability enhancement by integration of experimental design and principal  
 component analysis,  
 Powder Technology, Volume 258, May 2014, Pages 331-343

**Table 2**  
 Responses of 3<sup>2</sup> full factorial design batches of TLM loaded nanosuspensions.

| Batch code | Particle size (nm) | Saturation solubility (µg/mL) | Polydispersibility index | Zeta potential (mV) |
|------------|--------------------|-------------------------------|--------------------------|---------------------|
| TLM-NS-F1  | 470.67 ± 10.60     | 1211.23 ± 54.73               | 0.18 ± 0.07              | -27.55 ± 2.67       |
| TLM-NS-F2  | 423.67 ± 8.43      | 2190.14 ± 76.56               | 0.18 ± 0.03              | -29.90 ± 3.78       |
| TLM-NS-F3  | 406.00 ± 4.65      | 2837.47 ± 98.54               | 0.13 ± 0.04              | -31.55 ± 5.61       |
| TLM-NS-F4  | 390.33 ± 6.87      | 3056.09 ± 101.66              | 0.18 ± 0.03              | -32.73 ± 3.67       |
| TLM-NS-F5  | 356.67 ± 8.40      | 4431.10 ± 114.70              | 0.10 ± 0.07              | -34.85 ± 6.52       |
| TLM-NS-F6  | 330.33 ± 6.88      | 4438.26 ± 109.78              | 0.12 ± 0.02              | -35.76 ± 1.55       |
| TLM-NS-F7  | 424.00 ± 5.32      | 2630.13 ± 71.00               | 0.16 ± 0.02              | -30.63 ± 3.70       |
| TLM-NS-F8  | 386.00 ± 8.43      | 3073.91 ± 96.12               | 0.15 ± 0.04              | -32.46 ± 6.54       |
| TLM-NS-F9  | 367.33 ± 9.11      | 3876.25 ± 89.80               | 0.14 ± 0.02              | -32.10 ± 1.43       |

The results are mean ± SD (n = 3).

**Table 3**  
 Summary of ANOVA study for TLM loaded nanosuspensions.

| Particle size (Y <sub>1</sub> ) |                 |                  |                 |
|---------------------------------|-----------------|------------------|-----------------|
|                                 | DF <sup>a</sup> | SSR <sup>b</sup> | MS <sup>c</sup> |
| Regression                      |                 |                  |                 |
| FM <sup>d</sup>                 | 5               | 13,965.58        | 2793.12         |
| RM <sup>e</sup>                 | 4               | 13,953.33        | 3488.33         |
| Residual                        |                 |                  |                 |
| FM                              | 3               | 40.42            | 13.47           |
| RM                              | 4               | 52.67            | 13.17           |

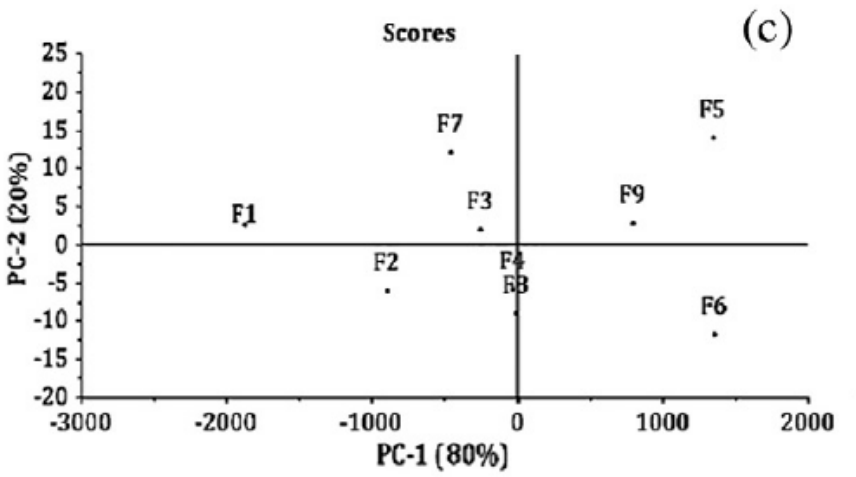
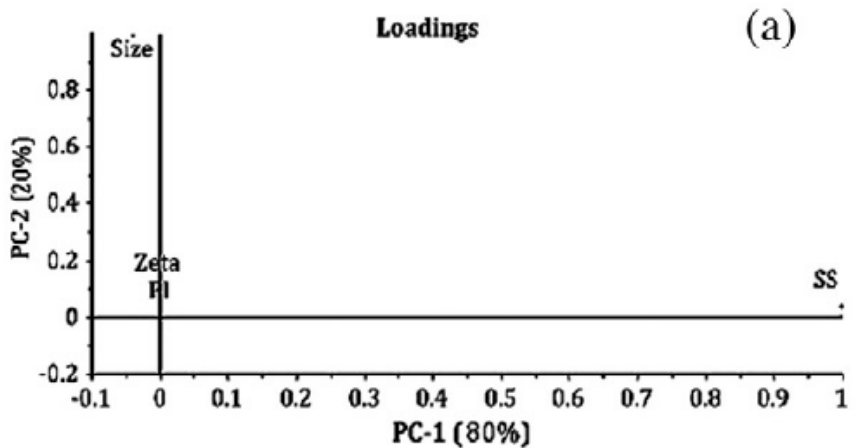
R<sup>2</sup> = 0.9962 Fcal = 0.91  
 Fcritical = 10.13 DF = (1, 3)

| Saturation solubility (Y <sub>2</sub> ) |    |           |           |
|---|----|-----------|-----------|
|   | DF | SSR       | MS        |
| Regression                              |    |           |           |
| FM                                      | 5  | 8,597,271 | 1,719,454 |
| RM                                      | 3  | 8,461,416 | 2,820,472 |
| Residual                                |    |           |           |
| FM                                      | 3  | 253,091.1 | 84363.7   |
| RM                                      | 5  | 388,946.7 | 77,789.33 |

R<sup>2</sup> = 0.9560 Fcal = 0.80  
 Fcritical = 9.55 DF = (2, 3)

<sup>a</sup> DF: Degree of freedom.  
<sup>b</sup> SSR: Sum of square residuals.  
<sup>c</sup> MS: Mean of squares.  
<sup>d</sup> FM: Full model.  
<sup>e</sup> RM: Reduced model.



Kevin C. Garala, Jaydeep M. Patel, Anjali P. Dhingani, Abhay T. Dharamsi, Preparation and evaluation of agglomerated crystals by crystallo-co-agglomeration: An integrated approach of principal component analysis and Box–Behnken experimental design, International Journal of Pharmaceutics, Volume 452, Issues 1–2, 16 August 2013, Pages 135-156

CCA: Cristallisation de l'API et agglomération avec les excipients.

3 variables sélectionnées après screening:

Ratio CH<sub>2</sub>Cl<sub>2</sub> / eau  
Concentration du PEG6000  
Vitesse d'agitation

**Table 1**  
Box–Behnken design batches.

| Batch code | Independent variables       |                             |                             |
|------------|-----------------------------|-----------------------------|-----------------------------|
|            | X <sub>1</sub> <sup>a</sup> | X <sub>2</sub> <sup>b</sup> | X <sub>3</sub> <sup>c</sup> |
| R1         | -1                          | -1                          | 0                           |
| R2         | 1                           | -1                          | 0                           |
| R3         | -1                          | 1                           | 0                           |
| R4         | 1                           | 1                           | 0                           |
| R5         | -1                          | 0                           | -1                          |
| R6         | 1                           | 0                           | -1                          |
| R7         | -1                          | 0                           | 1                           |
| R8         | 1                           | 0                           | 1                           |
| R9         | 0                           | -1                          | -1                          |
| R10        | 0                           | 1                           | -1                          |
| R11        | 0                           | -1                          | 1                           |
| R12        | 0                           | 1                           | 1                           |
| R13        | 0                           | 0                           | 0                           |

| Factor   | Level |      |      |
|--|-------|------|------|
|  | -1    | 0    | 1    |
| X <sub>1</sub> (DCM: water)                      | 0.04  | 0.07 | 1    |
| X <sub>2</sub> (Concentration of PEG 6000, %w/w) | 2     | 3.5  | 5    |
| X <sub>3</sub> (Speed, rpm)                      | 600   | 800  | 1000 |

# Kevin C. Garala, Jaydeep M. Patel, Anjali P. Dhingani, Abhay T. Dharamsi, Preparation and evaluation of agglomerated crystals by crystallo-co-agglomeration: An integrated approach of principal component analysis and Box–Behnken experimental design, International

Journal of Pharmaceutics, Volume 452, Issues 1–2, 16 August 2013, Pages 135-156

Results of evaluation parameters of pristine and agglomerated RCD.

| Batch <sup>a</sup>                    | RCD           | R1            | R2            | R3            | R4            | R5            | R6            |
|---------------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| dg <sup>a</sup> (mm)                  | 0.137 ± 0.103 | 0.697 ± 0.142 | 0.892 ± 0.139 | 0.725 ± 0.127 | 0.973 ± 0.116 | 1.009 ± 0.168 | 1.214 ± 0.193 |
| CS <sup>b</sup> (gm)                  | –             | 46.27 ± 3.66  | 35.41 ± 1.51  | 51.07 ± 2.69  | 42.18 ± 2.38  | 49.32 ± 2.75  | 39.24 ± 1.98  |
| SF <sup>c</sup>                       | 0.415 ± 0.052 | 0.826 ± 0.083 | 0.809 ± 0.067 | 0.901 ± 0.065 | 0.896 ± 0.073 | 0.938 ± 0.071 | 0.857 ± 0.053 |
| CI <sup>d</sup>                       | 39.48 ± 2.05  | 14.57 ± 1.29  | 17.84 ± 2.67  | 17.09 ± 1.68  | 15.43 ± 1.34  | 14.55 ± 1.06  | 17.73 ± 1.25  |
| %Y <sup>e</sup>                       | –             | 94.59 ± 2.07  | 88.17 ± 2.66  | 90.43 ± 1.92  | 96.25 ± 1.43  | 98.16 ± 2.61  | 91.64 ± 2.75  |
| AoR <sup>f</sup> (°)                  | 45.63 ± 3.65  | 23.81 ± 1.38  | 22.94 ± 2.07  | 19.07 ± 1.76  | 20.18 ± 1.59  | 18.59 ± 1.67  | 22.45 ± 0.98  |
| HR <sup>g</sup>                       | 1.613 ± 0.132 | 1.141 ± 0.011 | 1.176 ± 0.013 | 1.165 ± 0.014 | 1.154 ± 0.012 | 1.150 ± 0.013 | 1.205 ± 0.027 |
| CF <sup>h</sup>                       | 0.354 ± 0.038 | 1.015 ± 0.271 | 0.973 ± 0.184 | 0.991 ± 0.143 | 0.987 ± 0.156 | 1.089 ± 0.117 | 1.107 ± 0.128 |
| IF <sup>i</sup>                       | 2.017 ± 0.073 | 2.936 ± 0.115 | 2.975 ± 0.129 | 3.024 ± 0.134 | 3.066 ± 0.128 | 2.891 ± 0.119 | 3.032 ± 0.083 |
| Φ <sup>j</sup>                        | 0.075 ± 0.012 | 0.856 ± 0.107 | 0.832 ± 0.083 | 0.907 ± 0.074 | 0.883 ± 0.051 | 0.940 ± 0.087 | 0.895 ± 0.075 |
| DC <sup>k</sup> (%)                   | –             | 98.54 ± 1.62  | 99.35 ± 1.75  | 95.67 ± 1.23  | 100.23 ± 1.07 | 97.84 ± 1.68  | 97.17 ± 1.64  |
| MC <sup>l</sup> (%)                   | 0.324 ± 0.101 | 0.735 ± 0.134 | 0.864 ± 0.153 | 1.113 ± 0.203 | 1.011 ± 0.196 | 0.996 ± 0.173 | 0.965 ± 0.135 |
| a <sup>m</sup>                        | 17.455 ± 1.06 | 5.154 ± 0.638 | 9.457 ± 0.921 | 5.181 ± 0.315 | 5.378 ± 0.423 | 4.735 ± 0.437 | 6.348 ± 0.539 |
| 1/b <sup>m</sup>                      | 1.375 ± 0.073 | 0.752 ± 0.064 | 0.528 ± 0.027 | 0.441 ± 0.092 | 0.541 ± 0.078 | 0.994 ± 0.083 | 0.645 ± 0.035 |
| K <sup>n</sup>                        | 0.079 ± 0.015 | 0.974 ± 0.093 | 0.953 ± 0.084 | 0.931 ± 0.102 | 0.987 ± 0.113 | 1.025 ± 0.132 | 0.983 ± 0.064 |
| A <sup>o</sup>                        | 1.375 ± 0.073 | 0.752 ± 0.064 | 0.528 ± 0.027 | 0.441 ± 0.092 | 0.541 ± 0.078 | 0.994 ± 0.083 | 0.645 ± 0.035 |
| k <sup>o</sup>                        | 0.079 ± 0.015 | 0.974 ± 0.093 | 0.953 ± 0.084 | 0.931 ± 0.102 | 0.987 ± 0.113 | 1.025 ± 0.132 | 0.983 ± 0.064 |
| Py <sup>o</sup> (tons)                | 29.24 ± 1.83  | 1.711 ± 0.09  | 1.739 ± 0.12  | 2.020 ± 0.22  | 1.594 ± 0.08  | 1.516 ± 0.09  | 1.639 ± 0.17  |
| σ <sub>o</sub> <sup>o</sup>           | 9.746 ± 1.02  | 0.570 ± 0.16  | 0.579 ± 0.19  | 0.673 ± 0.17  | 0.531 ± 0.15  | 0.505 ± 0.18  | 0.546 ± 0.12  |
| ER <sup>p</sup> (%)                   | 4.453 ± 0.497 | 0.815 ± 0.165 | 0.731 ± 0.234 | 0.725 ± 0.186 | 0.697 ± 0.127 | 0.554 ± 0.201 | 0.735 ± 0.179 |
| TS <sup>q</sup> (kg/cm <sup>2</sup> ) | 1.253 ± 0.131 | 5.215 ± 0.652 | 4.942 ± 0.341 | 5.697 ± 0.763 | 6.015 ± 0.434 | 4.684 ± 0.372 | 5.248 ± 0.421 |

| Batch <sup>a</sup>                    | R7            | R8            | R9            | R10           | R11           | R12           | R13           |
|---------------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| dg <sup>a</sup> (mm)                  | 0.351 ± 0.083 | 0.723 ± 0.091 | 1.102 ± 0.104 | 1.175 ± 0.157 | 0.437 ± 0.113 | 0.566 ± 0.115 | 0.834 ± 0.138 |
| CS <sup>b</sup> (gm)                  | 47.01 ± 2.65  | 38.44 ± 2.83  | 58.89 ± 3.61  | 64.35 ± 3.89  | 43.73 ± 2.37  | 62.98 ± 3.95  | 61.58 ± 3.52  |
| SF <sup>c</sup>                       | 0.992 ± 0.084 | 0.970 ± 0.077 | 0.792 ± 0.052 | 0.876 ± 0.047 | 0.841 ± 0.061 | 0.912 ± 0.043 | 0.959 ± 0.051 |
| CI <sup>d</sup>                       | 16.33 ± 1.78  | 15.61 ± 0.92  | 14.05 ± 0.83  | 15.84 ± 1.29  | 15.56 ± 1.15  | 14.24 ± 0.83  | 14.74 ± 0.73  |
| %Y <sup>e</sup>                       | 91.07 ± 2.94  | 96.65 ± 1.32  | 97.35 ± 2.73  | 92.17 ± 1.61  | 89.83 ± 1.36  | 93.55 ± 2.83  | 97.23 ± 2.97  |
| AoR <sup>f</sup> (°)                  | 17.84 ± 1.32  | 17.06 ± 2.17  | 17.51 ± 1.38  | 21.23 ± 1.52  | 22.35 ± 1.13  | 18.97 ± 1.39  | 18.41 ± 1.26  |
| HR <sup>g</sup>                       | 1.154 ± 0.016 | 1.144 ± 0.015 | 1.096 ± 0.011 | 1.155 ± 0.014 | 1.143 ± 0.012 | 1.136 ± 0.011 | 1.128 ± 0.013 |
| CF <sup>h</sup>                       | 0.999 ± 0.135 | 0.989 ± 0.113 | 0.982 ± 0.126 | 0.974 ± 0.149 | 0.987 ± 0.134 | 0.993 ± 0.148 | 1.054 ± 0.117 |
| IF <sup>i</sup>                       | 3.112 ± 0.201 | 2.959 ± 0.124 | 2.872 ± 0.139 | 2.983 ± 0.097 | 3.013 ± 0.133 | 3.047 ± 0.116 | 2.981 ± 0.124 |
| Φ <sup>j</sup>                        | 0.999 ± 0.054 | 0.981 ± 0.037 | 0.728 ± 0.056 | 0.868 ± 0.048 | 0.876 ± 0.074 | 0.912 ± 0.063 | 0.965 ± 0.055 |
| DC <sup>k</sup> (%)                   | 98.42 ± 2.09  | 99.68 ± 1.48  | 97.75 ± 1.96  | 98.23 ± 1.93  | 101.03 ± 1.61 | 99.58 ± 1.37  | 98.24 ± 1.46  |
| MC <sup>l</sup> (%)                   | 0.935 ± 0.158 | 0.918 ± 0.127 | 0.815 ± 0.139 | 0.997 ± 0.162 | 0.834 ± 0.137 | 1.017 ± 0.193 | 0.973 ± 0.175 |
| a <sup>m</sup>                        | 9.366 ± 0.832 | 2.854 ± 0.261 | 7.656 ± 0.733 | 5.335 ± 0.342 | 2.806 ± 0.303 | 2.847 ± 0.376 | 3.739 ± 0.294 |
| 1/b <sup>m</sup>                      | 0.814 ± 0.054 | 0.969 ± 0.032 | 0.796 ± 0.051 | 0.640 ± 0.072 | 0.514 ± 0.061 | 0.624 ± 0.049 | 0.756 ± 0.051 |
| K <sup>n</sup>                        | 1.214 ± 0.083 | 0.995 ± 0.097 | 0.953 ± 0.108 | 0.941 ± 0.093 | 1.106 ± 0.112 | 0.967 ± 0.094 | 0.985 ± 0.082 |
| A <sup>o</sup>                        | 0.814 ± 0.054 | 0.969 ± 0.032 | 0.796 ± 0.051 | 0.640 ± 0.072 | 0.514 ± 0.061 | 0.624 ± 0.049 | 0.756 ± 0.051 |
| k <sup>o</sup>                        | 1.214 ± 0.083 | 0.995 ± 0.097 | 0.953 ± 0.108 | 0.941 ± 0.093 | 1.106 ± 0.112 | 0.967 ± 0.094 | 0.985 ± 0.082 |
| Py <sup>o</sup> (tons)                | 1.971 ± 0.09  | 1.437 ± 0.07  | 1.806 ± 0.15  | 1.462 ± 0.06  | 1.421 ± 0.07  | 1.208 ± 0.06  | 1.367 ± 0.08  |
| σ <sub>o</sub> <sup>o</sup>           | 0.656 ± 0.13  | 0.479 ± 0.11  | 0.604 ± 0.17  | 0.487 ± 0.15  | 0.473 ± 0.14  | 0.402 ± 0.16  | 0.455 ± 0.17  |
| ER <sup>p</sup> (%)                   | 0.836 ± 0.193 | 0.565 ± 0.152 | 0.468 ± 0.103 | 0.578 ± 0.118 | 0.549 ± 0.134 | 0.605 ± 0.156 | 0.765 ± 0.149 |
| TS <sup>q</sup> (kg/cm <sup>2</sup> ) | 5.367 ± 0.587 | 6.164 ± 0.832 | 5.654 ± 0.426 | 4.964 ± 0.319 | 5.548 ± 0.571 | 5.218 ± 0.385 | 5.584 ± 0.463 |

<sup>a</sup> Mean geometric diameter.

<sup>b</sup> Crushing strength.

<sup>c</sup> Shape factor.

<sup>d</sup> Carr's Index

<sup>e</sup> Percent yield.

<sup>f</sup> Angle of repose.

<sup>g</sup> Hausner ratio.

<sup>h</sup> Circularity factor

<sup>i</sup> Irregularity factor.

<sup>j</sup> Aspect ratio.

<sup>k</sup> Drug content.

<sup>l</sup> Moisture content.

<sup>m</sup> Kawakita parameters.

<sup>n</sup> Kuno's constant.

<sup>o</sup> Heckel parameters.

<sup>p</sup> Elastic recovery.

<sup>q</sup> Tensile strength.

<sup>r</sup> Results are mean of three determinations ±SD.



Kevin C. Garala, Jaydeep M. Patel, Anjali P. Dhingani, Abhay T. Dharamsi, Preparation and evaluation of agglomerated crystals by crystallo-co-agglomeration: An integrated approach of principal component analysis and Box–Behnken experimental design, International

Journal of Pharmaceutics, Volume 452, Issues 1–2, 16 August 2013, Pages 135-156

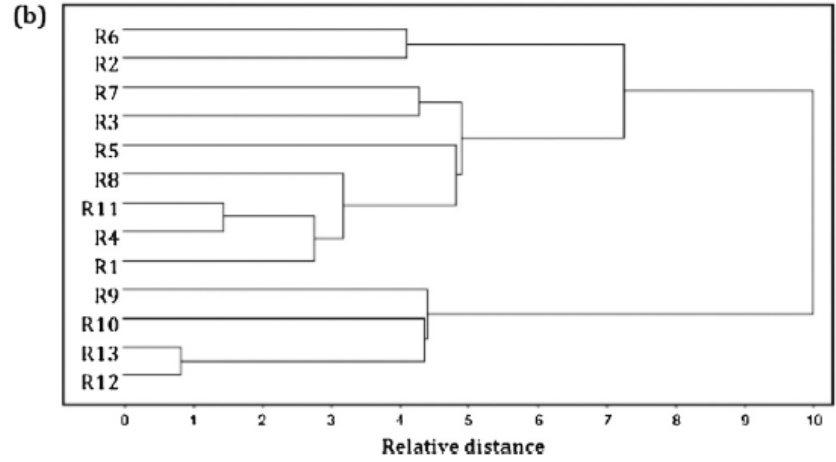
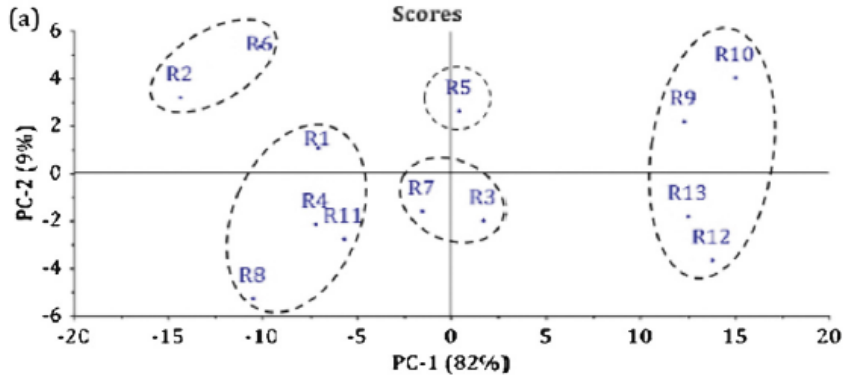


Fig. 3. Score plot from PCA (a) and Dendrogram from AHCA (b) of agglomerated RCD.

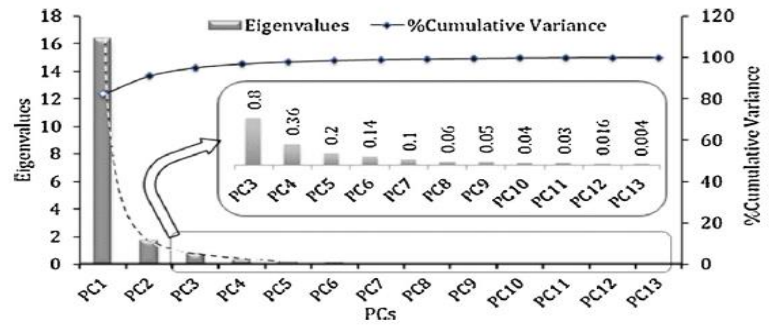
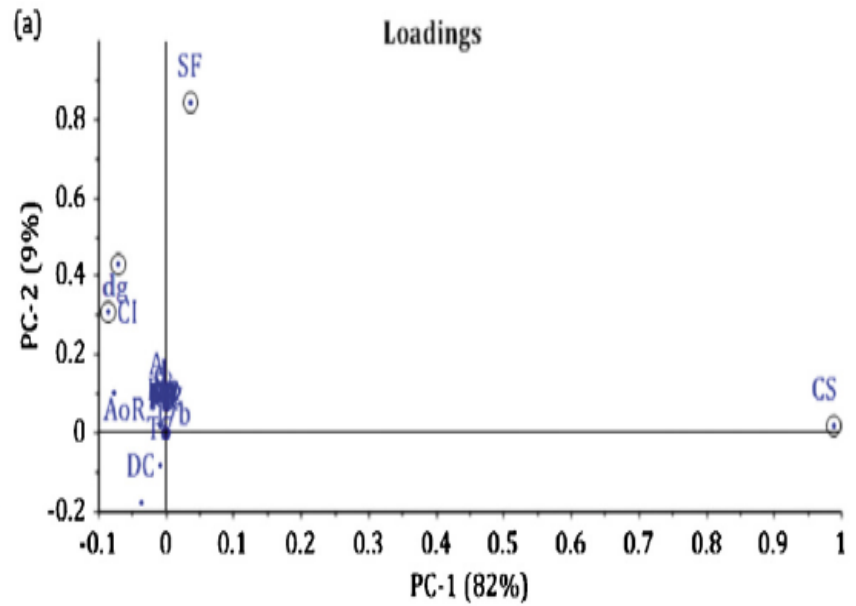
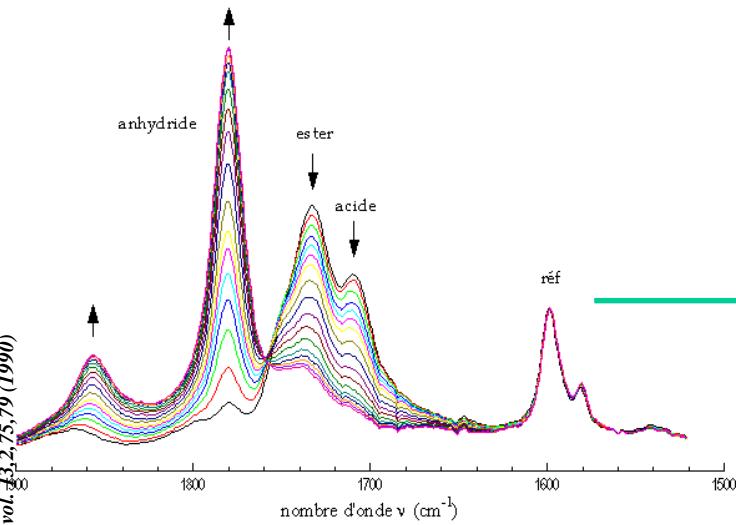


Fig. 7. Scree plot of all components with cumulative variance.

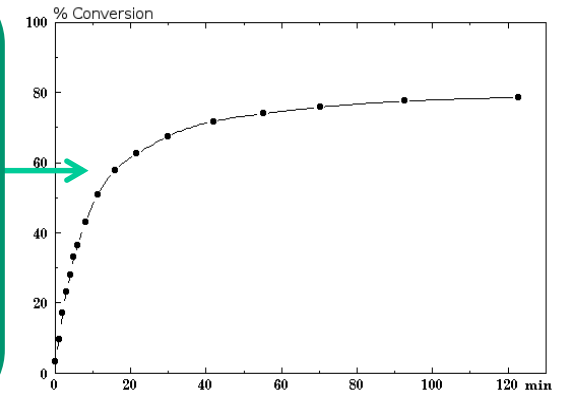
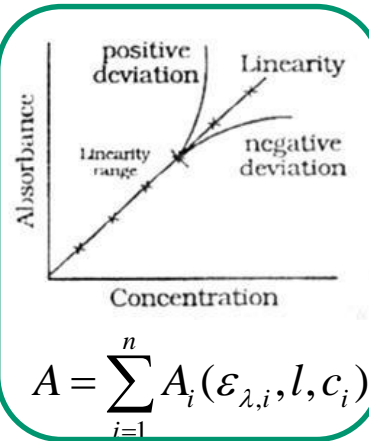


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# Hard vs soft modeling

- Modélisation « dure »



# Hard vs soft modeling

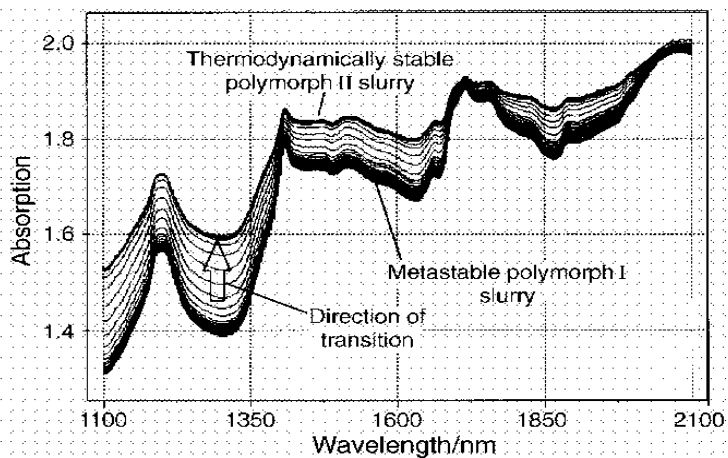
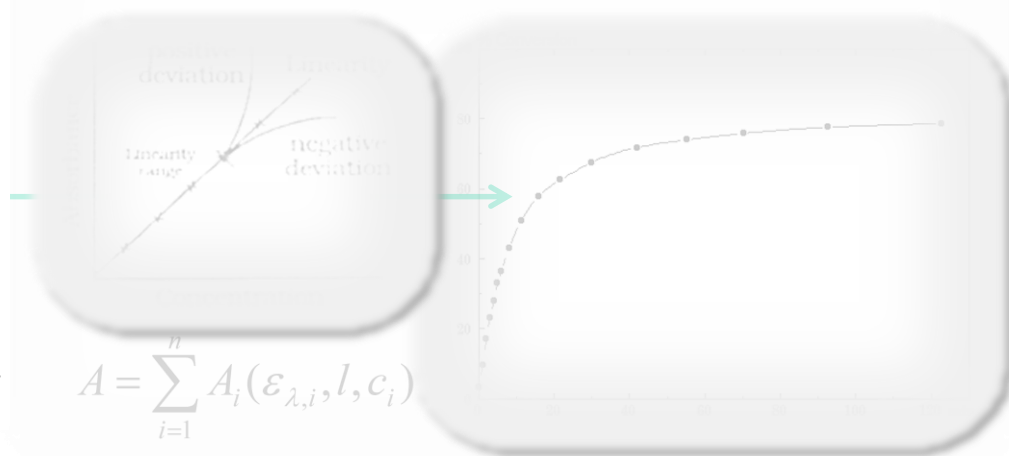


Fig. 2 Typical crystal slurry spectra collected during conversion of trovafloxacin mesylate polymorph I into polymorph II in butanol at 95 °C.

- Modélisation « dure »



$$A = \sum_{i=1}^n A_i(\epsilon_{\lambda,i}, l, c_i)$$



Modèle  
chimométrique  
multivarié

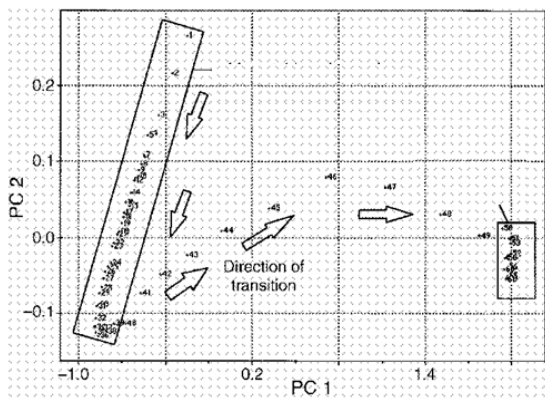


Fig. 3 Scores plot of principal component 1 (PC 1) versus principal component 2 (PC 2) for typical conversion.

- Modélisation  
« comportementale »  
ou « soft modeling ».

Timothy Norris, Paul K Aldridge and S. Sonja Sekulic.  
*Analyst* June 1997 vol 122 (549-552)

Hea-Eun Lee, Min-Jeong Lee, Woo-Sik Kim, Myung-Yung Jeong, Young-Sang Cho, Guang Jin Choi,  
 In-line monitoring and interpretation of an indomethacin anti-solvent crystallization process  
 by near-infrared spectroscopy (NIRS),  
 International Journal of Pharmaceutics, Volume 420, Issue 2, 28 November 2011, Pages  
 274-281

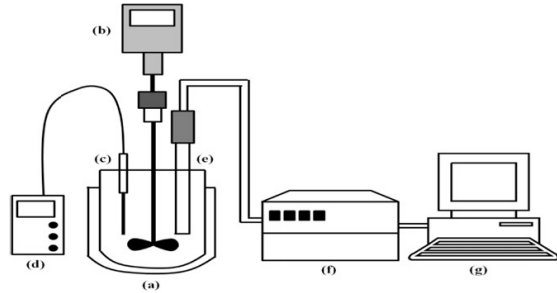


Fig. 1. A schematic diagram of experimental apparatus: (a) glass jacketed re (b) agitator, (c) temperature probe, (d) temperature indicator, (e) NIR fiber-optic probe, (f) NIR main body and (g) personal computer.

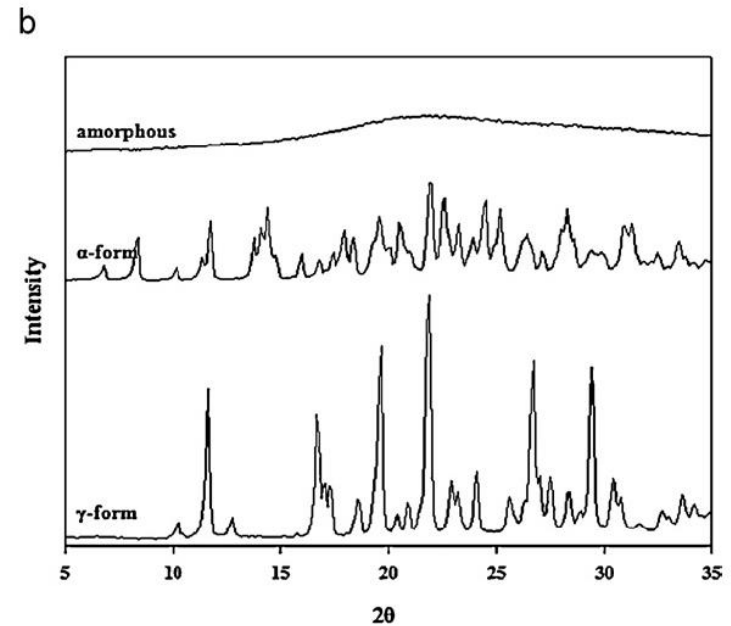
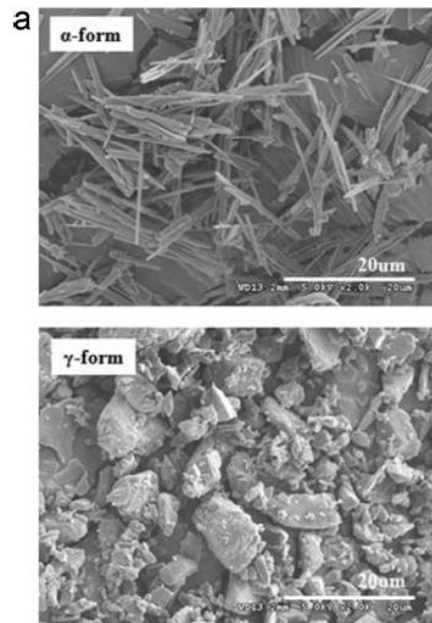


Fig. 2. SEM photographs and XRD patterns of standard IMC powders.

Hea-Eun Lee, Min-Jeong Lee, Woo-Sik Kim, Myung-Yung Jeong, Young-Sang Cho, Guang Jin Choi,  
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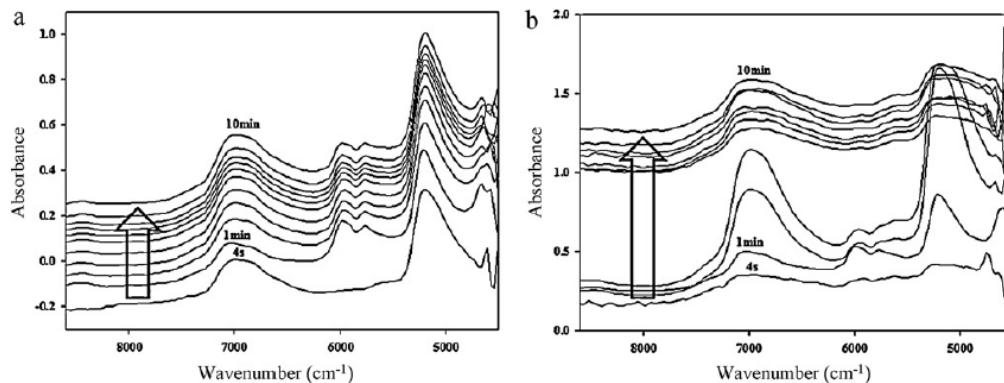


Fig. 3. NIR spectra acquired during IMC crystallization process (the first spectrum at 4 s and the rest 10 spectra at every minute from 1 to 10): (a) S-to-A scheme and (b) A-to-S scheme.

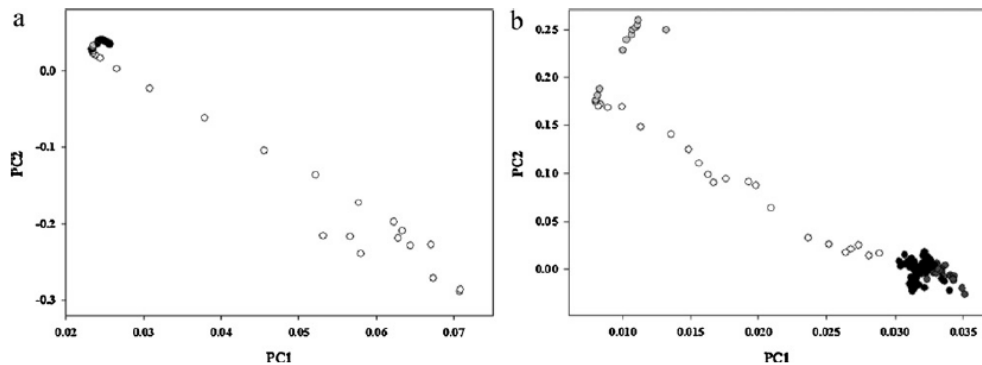


Fig. 4. PC score plots of IMC crystallization process: (a) S-to-A scheme and (b) A-to-S scheme.

“Although pure  $\alpha$ -form IMC powder was resulted under A-to-S scheme, a mixture of the  $\alpha$ -form and  $\gamma$ -form was produced for S-to-A case.”